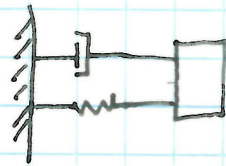


Review of Differential Equation Solution

Dynamics \rightarrow 2nd Order Universe $F = ma = m\ddot{x}$

Const. coeff's, homogeneous case

$$m\ddot{x} + c\dot{x} + kx = 0$$



$$\begin{aligned}x &= A e^{rt} \\ \dot{x} &= A r e^{rt} \\ \ddot{x} &= A r^2 e^{rt}\end{aligned}$$

$$(mr^2 + cr + k) A e^{rt} = 0$$

$$mr^2 + cr + k = 0, \text{ solve for } r$$

3 cases

Case 1: $r \rightarrow$ 2 roots, same: $r = r_1$, real

$$x = A_1 e^{r_1 t} + A_2 t e^{r_1 t}, \text{ w/ } A_1 \text{ and } A_2 \text{ solved from I.C.s}$$

Case 2: $r \rightarrow$ 2 roots, real, different, r_1, r_2 ,

$$x = A_1 e^{r_1 t} + A_2 e^{r_2 t}$$

Case 3: $r \rightarrow$ 2 roots, complex (imaginary components)

$$r = (\alpha + \omega i), (\alpha - \omega i)$$

$$x = A_1 e^{(\alpha + \omega i)t} + A_2 e^{(\alpha - \omega i)t}, \quad i = \sqrt{-1}, \quad A e^{i\omega t} = C \cos \omega t + i S \omega t$$

$e^{\alpha t} \downarrow e^{i\omega t}$

$$x = A_1 e^{\alpha t} [\cos(\omega t) + i \sin(\omega t)] + A_2 e^{\alpha t} [\cos(-\omega t) + i \sin(-\omega t)]$$

$$= \begin{matrix} \downarrow \\ \text{same} \end{matrix} + A_2 e^{\alpha t} [\cos(\omega t) - i \sin(\omega t)]$$

$$= (A_1 + A_2) e^{\alpha t} \cos(\omega t) + i(A_1 - A_2) e^{\alpha t} \sin(\omega t)$$

$$= A_1' e^{\alpha t} \cos(\omega t) + A_2' e^{\alpha t} i \sin(\omega t)$$

Assume:

$$A_1' = c\phi, A_2' = -s\phi$$

$$x = Ae^{\alpha t} (c\phi \cos \omega t - s\phi \sin \omega t)$$

$$\vec{x} = Ae^{\alpha t} \cos(\omega t + \phi)$$

Amplitude from I.C. \nearrow real term \nwarrow freq imaginary term \nwarrow phase shift, coefficient from I.C.

$$m\ddot{x} + \overset{0}{c}x + k = 0$$

$$mr^2 + k = 0, r = \pm \sqrt{-k/m} \quad \frac{k}{m} \text{ pos.}$$

Case 3: r is imaginary solution, real part = 0

$$\vec{x} = A \cos(\omega t + \phi)$$

$$m\ddot{x} + cx + k = 0$$

$$Ae^{\alpha t} \cos(\omega t + \phi)$$

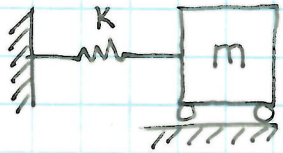
damping decay \nwarrow cyclical

Phase Portraits

Dynamics \rightarrow 2 ODE
 Rigid body 2 ODE
 flex.

Evaluate motion:

- closed form \rightarrow exact
- numerical solutions
- phase portrait

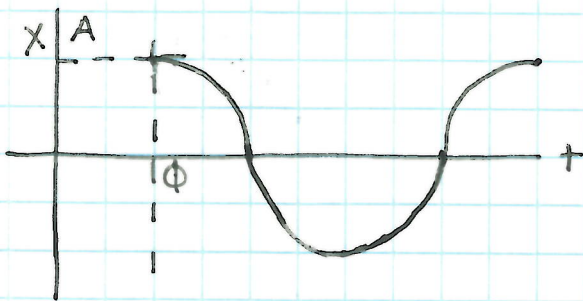


$$m\ddot{x} + kx = 0$$

$r \rightarrow 2$ imaginary

$$x = A \cos(\omega t + \phi) \leftarrow x(t)$$

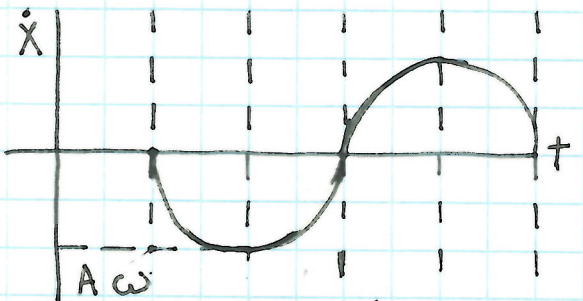
$$\dot{x} = -A\omega \sin(\omega t + \phi) \leftarrow \dot{x}(t)$$



x vs t

\dot{x} vs t

x vs \dot{x}

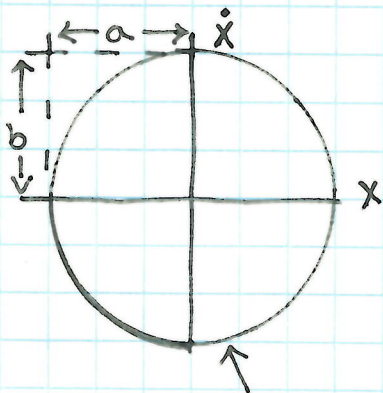


square and add

$$x^2 = A^2 \cos^2(\omega t + \phi)$$

$$+ \dot{x}^2 = A^2 \omega^2 \sin^2(\omega t + \phi)$$

$$x^2 + \frac{\dot{x}^2}{\omega^2} = A^2$$



$$Ax^2 + Cy^2 + Dx + Ey = F, \quad \underbrace{AC > 0, C \neq 0}_{\text{ellipse}}$$

$$Ac > 0$$

ellipse

$$\frac{(x-h)^2}{a^2} + \frac{(y-k)^2}{b^2} = 1 \quad (h, k) \text{ center} = (0, 0)$$

$$a = A, \quad b = A\omega$$

Phase Portrait
 solution to
 dynamics
 as x vs. \dot{x}

Phase Portraits cont.

Pros

- Alternate view
- Solve more exact
- Don't have to solve 2nd ODE

Cons

- solve / dof system
- certain cases: do not allow closed form solutions

→ Directly from EOM to Phase Portrait ←

① EOM → $m\ddot{x} + kx = 0$

② First integral of motion → $\int \text{EOM} = \int (m\ddot{x} + kx = 0) dx$

$$\int m\ddot{x} dx + \int kx dx = \int 0 dx$$

$$m \int \frac{dx}{dt} \frac{dx}{dt} + \frac{1}{2} kx^2 = E \text{ (constant)}$$

$$m \int d\dot{x} \frac{dx}{dt} + \frac{1}{2} kx^2 = E$$

$$m \int \dot{x} d\dot{x} + \frac{1}{2} kx^2 = E$$

$$\frac{1}{2} m\dot{x}^2 + \frac{1}{2} kx^2 = E \leftarrow \text{first integral of motion}$$

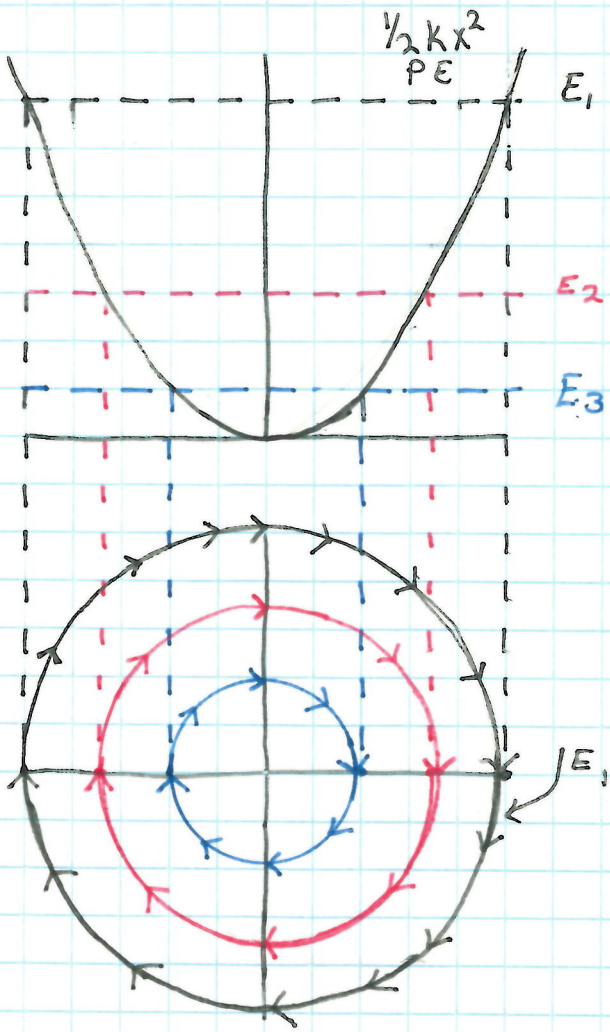
↳ response is an ellipse

- see that from my conic sections
- matlab
- third way → consider and plot each term

Third way: 1st integral of motion

$$\frac{1}{2} m\dot{x}^2 + \frac{1}{2} kx^2 = E$$

KE = T PE = V total E



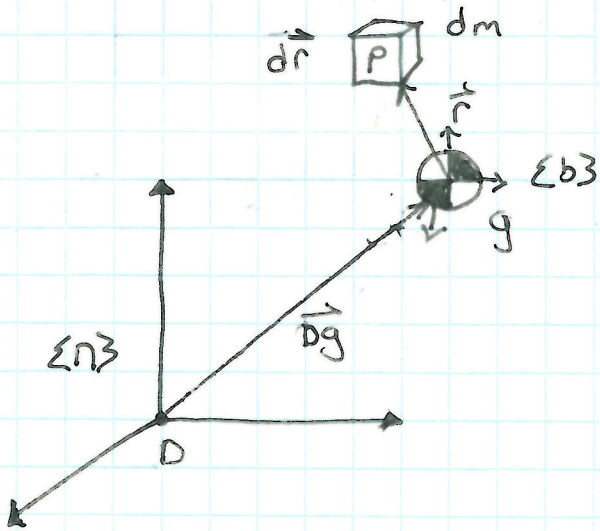
Direction:
 increasing $x \Rightarrow \dot{x} +$
 decreasing $x \Rightarrow \dot{x} -$

Newton-Euler Equations of motion

3-D, Rigid Bodies

N-2 \rightarrow EOM $\vec{F} = m\vec{a}$

Euler \rightarrow Extended N2 to Rigid Bodies



$$dF = \vec{a}_p dm$$

$$\int_{\text{body}} dF = \int_{\text{body}} \vec{a}_p dm$$

$$\vec{F} = \int_{\text{body}} \left(\frac{d^2}{dt^2} (\vec{D}g) + \frac{d^2}{dt^2} (\vec{r}) \right) dm$$

sum of all External Forces

$$= a_g \int_{\text{body}} dm + \int \left(\ddot{r} \hat{r} + \alpha \times \vec{r} + 2\dot{r} \omega - \omega \times (\omega \times \vec{r}) \right) dm$$

$$= a_g \int dm + \int \alpha \times \vec{r} dm + \int \omega \times (\omega \times \vec{r}) dm$$

$$\boxed{\vec{F} = m a_g} + 0 + 0$$

3, 2nd order
Differential
Equations of
motion

accel of C. of mass

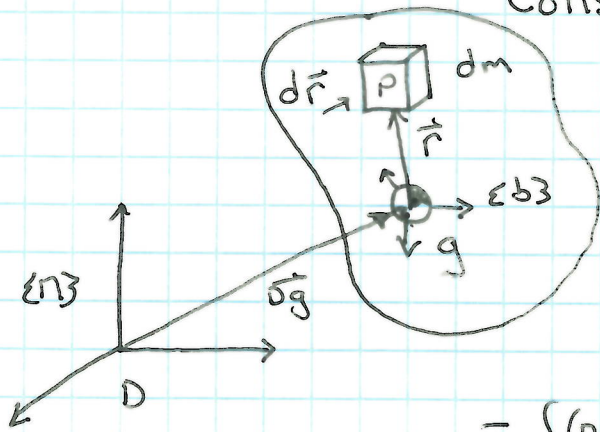
Center of mass = Center of gravity
* in uniform gravitational field

$$\sum F_x =$$

$$\sum F_y =$$

$$\sum F_z =$$

Newton-Euler Equations of motion Considering Moments



$$\vec{m} = \vec{r} \times dF$$

$$\int dm_D = \int_{\text{body}} \vec{D}_p \times dF = \int D_p \times \vec{\alpha}_p dm$$

$$m_D = \int (D_p) \times \vec{\alpha}_p dm$$

$$= \int (D_g + \vec{r}) \times (\vec{\alpha}_g + \vec{\alpha} \times \vec{r} + \vec{\omega} \times \vec{\omega} \times \vec{r}) dm$$

$$= \int \vec{D}_g \times \vec{\alpha}_g dm + \int \vec{D}_g \times \vec{\alpha} \times \vec{r} dm + \int \vec{D}_g \times \vec{\omega} \times \vec{\omega} \times \vec{r} dm$$

$$+ \int \vec{r} \times \vec{\alpha}_g dm + \int \vec{r} \times \vec{\alpha} \times \vec{r} dm + \int \vec{r} \times (\vec{\omega} \times (\vec{\omega} \times \vec{r})) dm$$

$$= \vec{D}_g \times \vec{\alpha}_g \int_{\text{body}} dm + \cancel{\vec{D}_g \times \vec{r} \times \int \vec{r} dm} + \cancel{\vec{D}_g \times \vec{\omega} \times (\vec{\omega} \times \int \vec{r} dm)} - \vec{\alpha}_g \times \int \vec{r} dm$$

$$+ \textcircled{A} + \textcircled{B}$$

\textcircled{A} $\int \vec{r} \times (\vec{\alpha} \times \vec{r}) dm$: triple vector Product "BAC - CAB" rule

$$\vec{A} \times \vec{B} \times \vec{C} \rightarrow \vec{B} (\vec{A} \cdot \vec{C}) - \vec{C} (\vec{A} \cdot \vec{B}), \text{ let } \vec{A} = \vec{r}, \vec{B} = \vec{\alpha}, \vec{C} = \vec{r}$$

$$\int (\vec{\alpha} (\vec{r} \cdot \vec{r}) dm - \vec{r} (\vec{r} \cdot \vec{\alpha}) dm$$

$$\vec{r} = r_1 \hat{b}_1 + r_2 \hat{b}_2 + r_3 \hat{b}_3$$

$$\alpha = \alpha_1 \hat{b}_1 + \alpha_2 \hat{b}_2 + \alpha_3 \hat{b}_3$$

$$= \int [(\alpha_1 \hat{b}_1 + \alpha_2 \hat{b}_2 + \alpha_3 \hat{b}_3)(x^2 + y^2 + z^2) - (x \hat{b}_1 + y \hat{b}_2 + z \hat{b}_3)(x\alpha_1 + y\alpha_2 + z\alpha_3)] dm$$

$$[\alpha_1 (x^2 + y^2 + z^2) - x^2 \alpha_1 - xy \alpha_2 - xz \alpha_3] \hat{b}_1$$

$$[\alpha_2 (x^2 + y^2 + z^2) - yx \alpha_1 - y^2 \alpha_2 - yz \alpha_3] \hat{b}_2$$

$$[\alpha_3 (x^2 + y^2 + z^2) - zx \alpha_1 - 2yz \alpha_2 - z^2 \alpha_3] \hat{b}_3$$

$$\int \vec{r} \times (\vec{\alpha} \times \vec{r}) dm = \int \begin{bmatrix} y^2+z^2 & -xy & -xz \\ -xy & x^2+z^2 & -yz \\ -zx & -zy & x^2+y^2 \end{bmatrix} \begin{bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_3 \end{bmatrix} dm \quad \leftarrow \text{E b3 or body frame}$$

$$= \int \begin{bmatrix} \\ \\ \end{bmatrix} dm \begin{bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_3 \end{bmatrix} = \vec{\alpha} \int \begin{bmatrix} \\ \\ \end{bmatrix} dm$$

↑
inertia matrix
inertia tensor ↓

$$\int \begin{bmatrix} y^2+z^2 & -xy & -xz \\ -yx & x^2+z^2 & -yz \\ -zx & -zy & x^2+y^2 \end{bmatrix} dm$$

Moments of inertia:

$$I_{11}, I_{22}, I_{33}$$

$$\int (y^2+z^2) dm \quad \int (x^2+z^2) dm \quad \int (x^2+y^2) dm$$

Products of inertia:

$$I_{12} = I_{21} = -\int xy dm$$

$$I_{13} = I_{31} = -\int xz dm$$

$$I_{23} = I_{32} = -\int yz dm$$

$$\int \vec{r} \times (\vec{\alpha} \times \vec{r}) dm = \mathbf{I} \vec{\alpha}$$

* body fixed frame

ⓑ $= \int \vec{r} \times (\vec{\omega} \times (\vec{\omega} \times \vec{r})) dm \rightarrow$ Apply triple vector Prod. $\vec{A} = \vec{r}, \vec{B} = \vec{\omega}$
 $\vec{C} = (\vec{\omega} \times \vec{r})$

$$= \int \vec{\omega} (\vec{r} \cdot \vec{\omega} \times \vec{r}) - (\vec{\omega} \times \vec{r}) (\vec{r} \cdot \vec{\omega}) dm$$

$$\vec{r} \cdot \vec{\omega} \times \vec{r} = 0 \quad (\vec{\omega} \times \vec{r} \perp \vec{r})$$

$$= -\int (\vec{\omega} \times \vec{r}) (\vec{r} \cdot \vec{\omega}) dm = \vec{\omega} \times \int -\vec{r} (\vec{r} \cdot \vec{\omega}) dm$$

$$= \vec{\omega} \times \int [\underbrace{\vec{\omega} (\vec{r} \cdot \vec{r})}_{\text{add this term?} \rightarrow 0} - \vec{r} (\vec{r} \cdot \vec{\omega})] dm$$

Apply triple vector Prod., $\bar{A} = \bar{r}$, $\bar{B} = \bar{\omega}$, $C = \bar{r}$

$$\bar{\omega} (\bar{r} \cdot \bar{r}) = \bar{B} (\bar{A} \cdot \bar{C}), \quad \bar{r} (\bar{r} \cdot \bar{\omega}) = \bar{C} (\bar{A} \cdot \bar{B})$$

$$\bar{\omega} \times \int \bar{r} (\bar{\omega} \times \bar{r}) dm$$

From before: $\int \bar{r} \times (\bar{\alpha} \times \bar{r}) dm \rightarrow \underline{I} \bar{\alpha}$

so now: $\int \bar{r} \times \bar{\omega} \times \bar{r} dm \rightarrow \underline{I} \bar{\omega}$

$$\textcircled{B} \int \bar{r} \times (\bar{\omega} (\bar{\omega} \times \bar{r})) dm \rightarrow \bar{\omega} \times \underline{I} \bar{\omega}$$

Pull it all together:

$$\boxed{\vec{m}_0 = m(\bar{D}_g \times \bar{a}_g) + \underline{I} \bar{\alpha} + \bar{\omega} \times \underline{I} \bar{\omega}} \leftarrow \text{Euler's rotational Equations}$$

Newton / Euler Eqns:

$$\sum F = m \bar{a}_g \leftarrow \text{sum of external forces}$$

$$\sum m_0 = m(\bar{D}_g \times \bar{a}_g) + \underset{\substack{\uparrow \\ \text{Inertia matrix} \\ \text{about } g.}}{\underline{I}_g} \bar{\alpha} + \bar{\omega} \times \underset{\substack{\uparrow \\ g}}{\underline{I}_g} \bar{\omega} \leftarrow \text{sum of external moments about a point}$$

g is the center of mass

\underline{I} is about g \leftarrow body fixed frame

$\bar{\omega}, \bar{\alpha}$ written in body fixed frame

Summary: Newton Euler Equations

$$\vec{F} = m \vec{a}_g$$

I_g about centroid

$$\vec{M}_0 = \vec{D}_g \times m \vec{a}_g + I \vec{\alpha} + \vec{\omega} \times I \vec{\omega} \quad \vec{\alpha}, \vec{\omega}, I \rightarrow \text{body fixed coords}$$

2 special cases: $D=g$ D is @ center of mass, $\vec{D}_g = 0$

$$\vec{m}_g = I_g \vec{\alpha} + \vec{\omega} \times I_g \vec{\omega}$$

D is fixed point

$$\vec{M}_0 = I_{F0} \vec{\alpha} + \vec{\omega} \times I_{F0} \vec{\omega}$$

Expand into Matrix form: $\vec{m}_g = I_g \vec{\alpha} + \vec{\omega} \times I_g \vec{\omega}$

$$\begin{bmatrix} m_1 \\ m_2 \\ m_3 \end{bmatrix} = \begin{bmatrix} I_{11} & I_{12} & I_{13} \\ I_{21} & I_{22} & I_{23} \\ I_{31} & I_{32} & I_{33} \end{bmatrix} \begin{bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_3 \end{bmatrix} + \begin{bmatrix} 0 & \omega_3 & \omega_2 \\ \omega_3 & 0 & \omega_1 \\ \omega_2 & \omega_1 & 0 \end{bmatrix} \begin{bmatrix} I_{11} & I_{12} & I_{13} \\ I_{21} & I_{22} & I_{23} \\ I_{31} & I_{32} & I_{33} \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}$$

↑

body fixed coord

↑

$$\vec{F} = m \vec{a}_g$$

$$\begin{bmatrix} F_1 \\ F_2 \\ F_3 \end{bmatrix} = m \begin{bmatrix} a_{g1} \\ a_{g2} \\ a_{g3} \end{bmatrix}$$

3, 2nd ORDER D.E.

↳ DOF rigid body

↳ 2nd Order D.E.s

-or-

12 1st order D.E.s

$3 \times 2 + 3 = 9$ 1st order Des

- Need 12 -

Euler Angular Eqn's

- set of 3 1st order D.E.s that come from Euler angles

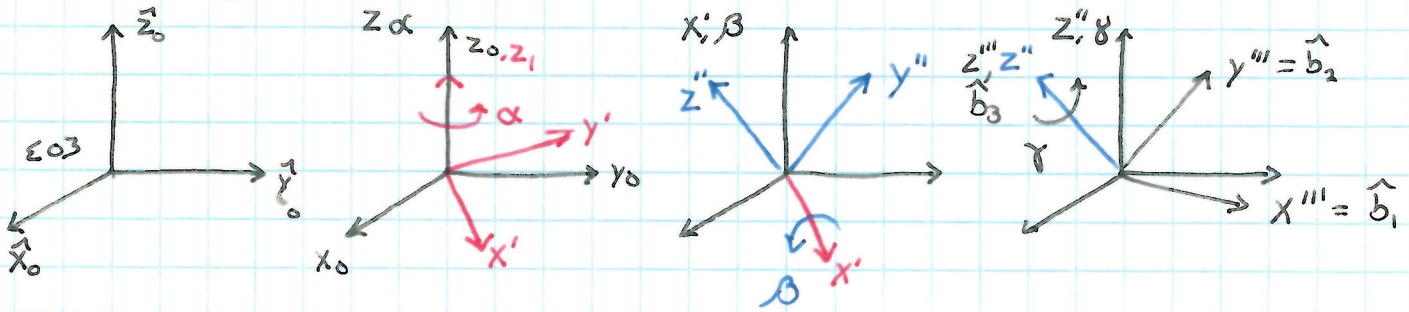
Euler Angular Equations

remaining 3 1st ODEs

- or -

Differential Equations From Euler's Angles

Euler's Angles for 313 α, β, γ Euler set:



3 additional 1st order Eqs.

- Use a specific Euler Angle Set
- Define D.E.s from this

$$R_{313}^{\alpha\beta\gamma} = R_b^n = R_{z\alpha} * R_{x\beta} * R_{z\gamma}$$

$$R_I^n * R_{II}'' * R_{III}'''$$

$${}^n \bar{\omega}^b = \dot{\alpha} \hat{z}' + \dot{\beta} \hat{x}'' + \dot{\gamma} \hat{b}_3$$

\uparrow z'', z'''

$$R_I^b \dot{\alpha} \hat{z}' + R_{II}^b \dot{\beta} \hat{x}'' + \dot{\gamma} \hat{b}_3$$

$$R_I^n = \begin{bmatrix} c\alpha & -s\alpha & 0 \\ s\alpha & c\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_{II}^I = \begin{bmatrix} 1 & 0 & 0 \\ 0 & c\beta & -s\beta \\ 0 & s\beta & c\beta \end{bmatrix}$$

$$R_{III}^{II} = \begin{bmatrix} c\gamma & -s\gamma & 0 \\ s\gamma & c\gamma & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\downarrow \begin{bmatrix} c\gamma & -s\gamma & 0 \\ c\beta s\gamma & c\beta c\gamma & -s\beta \\ s\beta s\gamma & s\beta c\gamma & c\beta \end{bmatrix}$$

$${}^n \bar{\omega}^b = R_b^{IT} \dot{\alpha} \hat{z}' + R_b^{II T} \dot{\beta} \hat{x}'' + \dot{\gamma} \hat{b}_3$$

$$= \begin{bmatrix} c\gamma & c\beta s\gamma & s\beta s\gamma \\ -s\gamma & c\beta c\gamma & s\beta c\gamma \\ 0 & -s\beta & c\beta \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ \dot{\alpha} \end{bmatrix} + \begin{bmatrix} c\gamma & s\gamma & 0 \\ -s\gamma & c\gamma & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\beta} \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \dot{\gamma} \end{bmatrix}$$

$${}^n \bar{\omega}^b = \begin{bmatrix} s_\beta s_\gamma \dot{\alpha} \\ s_\beta c_\gamma \dot{\alpha} \\ c_\beta \dot{\alpha} \end{bmatrix} + \begin{bmatrix} c_\gamma \dot{\beta} \\ -s_\gamma \dot{\beta} \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \dot{\gamma} \end{bmatrix}$$

$${}^n \bar{\omega}^b = \begin{bmatrix} s_\beta s_\gamma \dot{\alpha} + c_\gamma \dot{\beta} \\ s_\beta c_\gamma \dot{\alpha} - s_\gamma \dot{\beta} \\ c_\beta \dot{\alpha} + \dot{\gamma} \end{bmatrix} = \begin{bmatrix} s_\beta s_\gamma & c_\gamma & 0 \\ s_\beta c_\gamma & -s_\gamma & 0 \\ c_\beta & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \\ \dot{\gamma} \end{bmatrix}$$

$$\begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \\ \dot{\gamma} \end{bmatrix} = \underline{D}^{-1} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}^b \quad * \text{ Remaining 3, 1st order D.E.}$$

← Euler angular Eqns

Properties of Inertia Matrix

$$I = \begin{bmatrix} I_{11} & I_{12} & I_{13} \\ I_{21} & I_{22} & I_{23} \\ I_{31} & I_{32} & I_{33} \end{bmatrix}$$

← mass moment of inertia

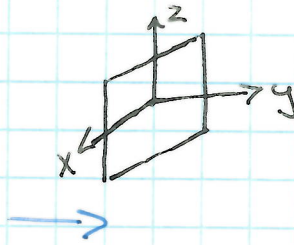
m = inertia, I_i = distribution of m about coord' axes.

Cat 1 moments of inertia

$$I_{xx} = I_{11} = \int (y^2 + z^2) dm$$

$$I_{yy} = I_{22} = \int (x^2 + z^2) dm$$

$$I_{zz} = I_{33} = \int (x^2 + y^2) dm$$



$$I = \begin{bmatrix} \text{moments} \\ \text{prod} \end{bmatrix}$$

Cat 2 Products of inertia symmetric

$$I_{xy} = I_{12} = I_{21} = - \int xy dm$$

$$I_{xz} = I_{13} = I_{31} = - \int xz dm$$

$$I_{yz} = I_{23} = I_{32} = - \int yz dm$$

I is Positive Definite Matrix

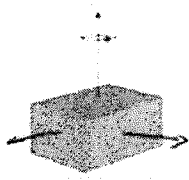
$$\bar{v}^T I \bar{v} > 0 \quad \text{for any non-zero } \bar{v}, \quad T_{\text{kinetic}}$$

$$\omega \rightarrow I \rho \Rightarrow I + \text{eigen values}$$

describe $I \rightarrow$ body fixed coords about C.g.

3 ways:

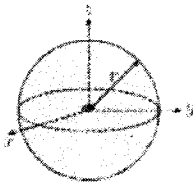
- 1) integration \rightarrow simple shapes
- 2) CAD \rightarrow properties
- 3) by book Typical shapes



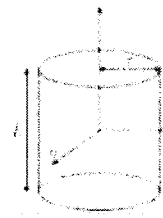
$$I_x = \frac{m}{12} (w^2 + d^2)$$

$$I_y = \frac{m}{12} (d^2 + h^2)$$

$$I_z = \frac{m}{12} (w^2 + h^2)$$

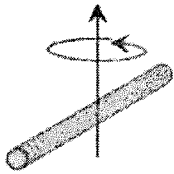


$$I = \frac{2mr^2}{5}$$

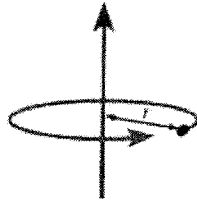


$$I_z = \frac{mr^2}{2}$$

$$I_x = I_y = \frac{m}{12} (3r^2 + h^2)$$



$$I_{\text{center}} = \frac{mL^2}{12}$$



$$I = mr^2$$



$$I_z = \frac{m}{5} (b^2 + c^2)$$

$$I_x = \frac{m}{5} (a^2 + c^2)$$

$$I_y = \frac{m}{5} (a^2 + b^2)$$

Parallel axis theorem.

$$I_{Gxx} = I_{gxx} + md^2 \leftarrow \text{translating by } d$$

Rotated axis Transformation; Describe $I_{\mathcal{E}b3} \rightarrow$ now $I_{\mathcal{E}n3}$
type similarity transform

$$\underline{I_n} = \underline{R}_b^n \underline{I}_b (\underline{R}_b^n)^T$$

Consider R. axis T. \rightarrow general I

$$I_{\text{gen}} = \begin{bmatrix} I_{11} & I_{21} & I_{31} \\ I_{12} & I_{22} & I_{32} \\ I_{13} & I_{23} & I_{33} \end{bmatrix}_{\text{gen}} \quad \rightarrow \quad I_p = \begin{bmatrix} I_{11p} & 0 & 0 \\ 0 & I_{22p} & 0 \\ 0 & 0 & I_{33p} \end{bmatrix}$$

Principle I - one in which the moments of inertia are the principle moments of inertia
Products of I $\Rightarrow 0$

$$I_p = R_{\star} I_{\text{gen}} R_{\star}^T$$

R_{\star} from Eigen value problem:
where $I_p \rightarrow$ eigen values (λ)

$R_{\star} \rightarrow$ Eigen vectors

In general \rightarrow Principle I through g. described in $\mathcal{E}b3$
principle components \rightarrow extremum.

\rightarrow define symmetry

directions \rightarrow directions

bodies w/ symmetry \rightarrow better stability under spin.

\downarrow better stability when spin is about
Principle directions

Euler's rotational Equations for principle I

$$\vec{M}_g = \underline{I}_g \vec{\alpha} + \vec{\omega} \times \underline{I}_g \vec{\omega}$$

$$\begin{bmatrix} m_1 \\ m_2 \\ m_3 \end{bmatrix} = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \begin{bmatrix} \dot{\omega}_1 \\ \dot{\omega}_2 \\ \dot{\omega}_3 \end{bmatrix} + \begin{bmatrix} 0 & \omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix} \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}$$

$$m_1 = I_1 \dot{\omega}_1 - (I_2 - I_3) \omega_2 \omega_3$$

$$m_2 = I_2 \dot{\omega}_2 - (I_3 - I_1) \omega_3 \omega_1$$

$$m_3 = I_3 \dot{\omega}_3 - (I_1 - I_2) \omega_1 \omega_2$$

Euler's Rotational Eqs
Principle Directions
about $\{b\}$

$$\dot{\omega}_1 = \frac{(I_2 - I_3) \omega_2 \omega_3}{I_1} + \frac{m_1}{I_1}$$

$$\dot{\omega}_2 = \frac{(I_3 - I_1) \omega_3 \omega_1}{I_2} + \frac{m_2}{I_2}$$

$$\dot{\omega}_3 = \frac{(I_1 - I_2) \omega_1 \omega_2}{I_3} + \frac{m_3}{I_3}$$

READY TO INTEGRATE

3 1st order D.E.

Euler's Rotat.
Egns

Euler's Angular
Egn.

313, α, β, δ

$$\begin{bmatrix} \dot{\alpha} \\ \dot{\beta} \\ \dot{\delta} \end{bmatrix} = \underline{D}^{-1} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}$$

$$\omega/D = \begin{bmatrix} s\beta s\delta & c\delta & 0 \\ s\beta c\delta & -s\delta & 0 \\ c\beta & 0 & 1 \end{bmatrix}$$